### CONFIDENTIAL



### UNIVERSITI TUN HUSSEIN ONN MALAYSIA

### FINAL EXAMINATION SEMESTER II SESSION 2013/2014

| COURSE NAME         | :     | REINFORCED CONCRETE DESIGN I   |
|---------------------|-------|--|
| COURSE CODE         | :     | BFC 32102  |
| PROGRAMME           | :     | 3 BFF  |
| EXAMINATION DATE    | :     | JUNE 2014  |
| DURATION            | :     | 2 HOURS 30 MINUTES   |
| INSTRUCTION         | :     | ANSWER <b>ALL</b> QUESTIONS FROM<br><b>SECTION A</b> AND <b>TWO (2)</b><br>QUESTIONS FROM <b>SECTION B</b><br>DESIGN SHOULD BE BASED ON: |
|                     |       | BS EN 1990:2002+A1:2005  |
|                     |       | NA BS EN 1990:2002+A1:2005   |
|                     |       | BS EN 1991-1-1:2002  |
|                     |       | NA BS EN 1991-1-1:2002   |
|                     |       | BS EN 1992-1-1:2004  |
|                     |       | BS 8110:PART 1:1997  |
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#### **SECTION A**

Q1 (a) Explain the fundamental assumptions that have been made in flexural theory of reinforced concrete design.

(4 marks)

(b) In elastic analysis, some of elastic moment at support can be reduced. Describe the purpose of moment redistribution especially in beam-column connections.

(4 marks)

- (c) A cross section of reinforced concrete beam is 250 x 450 mm as shown in Figure Q1. The tension and compression reinforcements provided are 4H25 and 2H16 respectively.
  - (i) Draw the simplified rectangular stress and strain block for the cross section beam in ultimate limit state.

(6 marks)

(ii) Based on the simplified rectangular stress block, determine the ultimate moment resistance of the section, if  $f_{ck} = 30 \text{ N/mm}^2$  and  $f_{yk} = 500 \text{ N/mm}^2$ . The depth to compression reinforcement and tension reinforcement are 50 mm and 410 mm, respectively.

(12 marks)

(iii) Based on the simplified rectangular stress block, determine the strain for compression reinforcement of the beam.

(4 marks)

### **SECTION B**

Q2 Figure Q2 shows the plan view of slab-beam system in one building. Due to construction works, beam and a part of the slab has to act as a pre-cast concrete slab. Given;

| Slab thickness                 | =                                    | 125 mm                      |                |
|--------------------------------|--------------------------------------|-----------------------------|----------------|
| Beam size                      | =                                    | 250 mm x 500 mm             |                |
| Finishes                       | =                                    | $1.0 \text{ kN/m}^2$        |                |
| Ceiling                        | =                                    | $1.0 \text{ kN/m}^2$        |                |
| Weight of concrete             | =                                    | $25 \text{ kN/m}^3$         |                |
| 3 m height brickwall           | =                                    | $2.6 \text{ kN/m}^2$        |                |
| (entire building)              |                                      |                             |                |
| Characteristic variable actio  | on, $q_k$                            | = 3.0 kN/m <sup>2</sup>     |                |
| Characteristic. strength of co | ete, $f_{ck}$ = 25 N/mm <sup>2</sup> | ,                           |                |
| Characteristic strength of ste | eel, $f_{yk}$                        | $f_{yk} = 500 \text{ N/mm}$ | 1 <sup>2</sup> |

Referring to a simply supported beam A/1-3,

Q3 Figure Q3 shows the simply supported slab spanning in two directions. Given slab thickness is 220mm and the effective span in each direction is 4.0 m and 6.0 m respectively. The slab subjected to a variable action of 15kN/m<sup>2</sup>. The characteristic material strength are  $f_{ck} = 25$  N/mm<sup>2</sup> and  $f_{yk} = 500$  N/mm<sup>2</sup>. Assume the C<sub>nom</sub>=35mm and diameter of reinforcement bar is 10 mm.

- (a) Calculate the ultimate load of the slab.
  (b) Determine moment for both direction of slab.
  (c) Design the required reinforcement for both direction slabs.
  (d) Check the A<sub>s,min</sub> and A<sub>s.max</sub> with A<sub>s,prov</sub>.
  (a) Sketch the arrangement of reinforcement of slab.
  (b) (5 marks)
- Q4 Figure Q4(a) shows a continuous beam with each span length is 8m. Given, the total permanent action and the total variable action for the beam is 22.5kN/m and 10kN/m.
  - (a) By using Simplified Method, draw the diagram for bending moment and shear force for the beam.

(b) Design a T section for critical part of the beam based on the analysis in 4(a). The beam cross section is shown in Figure Q4(b). Given the characteristic material strength are  $f_{yk}$ = 500N/mm<sup>2</sup> and  $f_{ck}$ = 30N/mm<sup>2</sup>. Assume x=0.45d. (Hint: use stress block to lead you with the solution)

(25 marks)

### -END OF QUESTIONS-







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### FORMULA

| if $d'/x \le 0.38$ or                         |
|---|
| if $d'/x > 0.38$                              |
|   |
|   |
|   |
|   |
|   |
| $(0.567f_{ck})(b_{eff} - b_w)h_f(d - 0.5h_f)$ |
|   |
|   |
|   |
|   |

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# Table 1: Shear force coefficient for uniformly loaded rectangular panels supported on four sides with provision for torsion at corner (Source: Table 3.15, *BS EN 1992 -1-2*)

| Type of panel and location  | $\beta_{\rm rx}$ for values of $l_{\rm y}/l_{\rm x}$ |      |      |      |      | βπ   |      |      |      |
|---|--|------|------|------|------|------|------|------|------|
|   | 1.0  | 1.1  | 1.2  | 1.3  | 1.4  | 1.5  | 1.75 | 2.0  | 1    |
| Four edges continuous   |  |      |      |      |      |      |      |      |      |
| Continuous edge   | 0.33   | 0.36 | 0.39 | 0.41 | 0.43 | 0.45 | 0.48 | 0.50 | 0.33 |
| One short edge<br>discontinuous                                   |  |      |      |      |      |      |      |      |      |
| Continuous edge   | 0.36   | 0.39 | 0.42 | 0.44 | 0.45 | 0.47 | 0.50 | 0.52 | 0.36 |
| Discontinuous edge  | _  | _    | -    | -    | —    | —    | _    | -    | 0.24 |
| One long edge<br>discontinuous                                    |  |      |      |      |      |      |      |      |      |
| Continuous edge   | 0.36   | 0.40 | 0.44 | 0.47 | 0.49 | 0.51 | 0.55 | 0.59 | 0.36 |
| Discontinuous edge  | 0.24   | 0.27 | 0.29 | 0.31 | 0.32 | 0.34 | 0.36 | 0.38 | -    |
| Two adjacent edges<br>discontinuous                               |  |      |      |      |      |      |      |      |      |
| Continuous edge   | 0.40   | 0.44 | 0.47 | 0.50 | 0.52 | 0.54 | 0.57 | 0.60 | 0.40 |
| Discontinuous edge  | 0.26   | 0.29 | 0.31 | 0.33 | 0.34 | 0.35 | 0.38 | 0.40 | 0.26 |
| Two short edges<br>discontinuous                                  |  |      |      |      |      |      |      |      |      |
| Continuous edge   | 0.40   | 0.43 | 0.45 | 0.47 | 0.48 | 0.49 | 0.52 | 0.54 | -    |
| Discontinuous edge  | _  | _    | -    | _    | —    | _    | —    | -    | 0.26 |
| Two long edges<br>discontinuous                                   |  |      |      |      |      |      |      |      |      |
| Continuous edge   | -  | _    | -    | -    | -    | -    | -    | -    | 0.40 |
| Discontinuous edge  | 0.26   | 0.30 | 0.33 | 0.36 | 0.38 | 0.40 | 0.44 | 0.47 | -    |
| Three edges<br>discontinuous<br>(one long edge<br>discontinuous)  |  |      |      |      |      |      |      |      |      |
| Continuous edge   | 0.45   | 0.48 | 0.51 | 0.53 | 0.55 | 0.57 | 0.60 | 0.63 | _    |
| Discontinuous edge  | 0.30   | 0.32 | 0.34 | 0.35 | 0.36 | 0.37 | 0.39 | 0.41 | 0.29 |
| Three edges<br>discontinuous<br>(one short edge<br>discontinuous) |  |      |      |      |      |      |      |      |      |
| Continuous edge   | _  | _    | -    | -    | -    | —    | -    | -    | 0.45 |
| Discontinuous edge  | 0.29   | 0.33 | 0.36 | 0.38 | 0.40 | 0.42 | 0.45 | 0.48 | 0.30 |
| Four edges<br>discontinuous                                       |  |      |      |      |      |      |      |      |      |
| Discontinuous edge  | 0.33   | 0.36 | 0.39 | 0.41 | 0.43 | 0.45 | 0.48 | 0.50 | 0.33 |

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# Table 2: Minimum dimensions and axis distances for reinforced and prestressed concrete simply supported one-way and two-way solid slabs (Source: Table 5.8 BS EN 1992 -1-2)

 Table 5.8 provides minimum values of axis distance to the soffit of simply supported slabs for standard fire resistances of R 30 to R 240,

(2) In two-way spanning slabs a denotes the axis distance of the reinforcement in the lower layer.

| Standard fire resistance | Minimum dimensions (mm)          |                 |  |     |  |  |  |
|--------------------------|----------------------------------|-----------------|--|-----|--|--|--|
|                          | slab                             | axis-distance a |  |     |  |  |  |
|                          | thickness<br>h <sub>s</sub> (mm) | one way         | two way:<br>$ J_{1} _{1,5} \le 1.5$ $ 1.5 <  J_{1} _{2} \le 1.5$ |     |  |  |  |
| 1                        | 2                                | 3               | 4  | 5   |  |  |  |
| REI 30                   | 60                               | 10*             | 10*  | 10* |  |  |  |
| REI 60                   | 80                               | 20              | 10*  | 15* |  |  |  |
| REI 90                   | 100                              | 30              | 15*  | 20  |  |  |  |
| REI 120                  | 120                              | 40              | 20   | 25  |  |  |  |
| REI 180                  | 150                              | 55              | 30   | 40  |  |  |  |
| REI 240                  | 175                              | 65              | 40   | 50  |  |  |  |

 $l_x$  and  $l_y$  are the spans of a two-way slab (two directions at right angles) where  $l_y$  is the longer span.

For prestressed slabs the increase of axis distance according to 5.2(5) should be noted.

The axis distance *a* in Column 4 and 5 for two way slabs relate to slabs supported at all four edges. Otherwise, they should be treated as one-way spanning slab.

\* Normally the cover required by EN 1992-1-1 will control.

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## Table 3: Design ultimate bending moments and shear forces(Source: Table 3.5, BS 8110 -1: 1997)

|        | At outer<br>support | Near<br>middle of<br>end span | At first<br>interior<br>support | At middle of<br>interior<br>spans | At interior<br>supports |
|--------|---------------------|-------------------------------|---------------------------------|-----------------------------------|-------------------------|
| Moment | 0                   | 0.09 <i>Fl</i>                | -0.11 <i>Fl</i>                 | 0.07 <i>Fl</i>                    | -0.08 <i>Fl</i>         |
| Shear  | 0.45F               | -                             | <b>0.6</b> <i>F</i>             | -                                 | 0.55F                   |

NOTE: *l* is the effective span;

*F* is the total design ultimate load  $(1.35G_k + 1.5 Q_k)$ 

No redistribution of the moment calculated from this table should be made.

### Table 4: Ultimate bending moment and shear force in one-way spanning slabs(Source: Table 3.5, BS 8110 -1: 1997)

|        | En                  | d support/s                      | lab connect         | At first<br>interior             | Middle<br>interior  | Interior<br>supports |          |
|--------|---------------------|----------------------------------|---------------------|----------------------------------|---------------------|----------------------|----------|
|        | Sin                 | nple                             | Continuous          |                                  |                     |                      |          |
|        | At outer<br>support | Near<br>middle<br>of end<br>span | At outer<br>support | Near<br>middle<br>of end<br>span | support spa         | spans                |          |
| Moment | 0                   | 0.086Fl                          | -0.04 <i>Fl</i>     | 0.075 <i>Fl</i>                  | -0.086Fl            | 0.063Fl              | -0.063Fl |
| Shear  | 0.45F               | -                                | 0.46F               | -                                | <b>0.6</b> <i>F</i> | -                    | 0.5F     |

NOTE: *l* is the effective span;

*F* is the total design ultimate load  $(1.35G_k + 1.5 Q_k)$ 

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# Table 5: Bending moment coefficients for slabs spanning in two directions at right angles,simply-supported on four sides (Sources: Table 3.13, BS8110:1:1997)

| $l_{\rm y}/l_{\rm x}$ | 1.0   | 1.1   | 1.2   | 1.3   | 1.4   | 1.5   | 1.75  | 2.0   |
|-----------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| $\alpha_{sx}$         | 0.062 | 0.074 | 0.084 | 0.093 | 0.099 | 0.104 | 0.113 | 0.118 |
| $\alpha_{sy}$         | 0.062 | 0.061 | 0.059 | 0.055 | 0.051 | 0.046 | 0.037 | 0.029 |